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IPC-TM-650 TEST METHODS MANUAL

1 Scope This test method is used to characterize the effects of flux residues on electrical performance by determining the degradation of electrical insulation resistance under conditions of high temperature and humidity.

This method, in conjunction with the supporting documentation in IPC-J-STD-004, is intended to be equivalent to Telcordia Technologies GR-78-CORE, Section 13.1, (Corrosiveness of Soldering Fluxes) and is used primarily by telecommunications companies to qualify the candidate flux or solder paste.

2 Applicable Documents

IPC-J-STD-004 Requirements for Soldering Fluxes

IPC-A-600 Acceptability of Printed Board

GR-78-CORE Physical Design and Manufacture of Telecommunications Product - Telcordia Technologies (Formerly Bellcore)

ASTM D-257 Standard Test Methods for DC Resistance or Conductance of Insulating Materials

2.1 Master Drawings

Telcordia Technologies Test Pattern (GR-78-CORE, Figures 14.1 and 14.2)

IPC-A-25A Multipurpose 1-sided Test Pattern

IPC-A-50 Surface Insulation Resistance Phoenix Board

3 Test Specimens The test specimens for this test method may be either of the interdigitated comb pattern shown in Figures 1 or 2.

These test patterns can be produced in a number of formats. Both of these patterns can be found on the IPC-B-50 Standard Test Board. The pattern shown in Figure 2 can be found on the IPC-B-25A test board (pattern D). Artwork for manufacturing these boards is available through the master drawings listed in 2.1. Contact IPC for a listing of vendors providing prefabricated test boards.

The comb pattern in Figure 1 has 0.65 mm [0.025 in] lines and 1.27 mm [0.050 in] spacings. This test pattern is also commonly referred to as the Bellcore pattern.

The comb pattern in Figure 2 has 0.32 mm [0.0125 in] lines and spaces (see Note 6.4).

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Subject	
Surface Insulation Resistance - Fluxes -	
Telecommunications	

Revision

Date

01/04

Originating Task Group

Surface Insulation Resistance Task Group, 5-32b

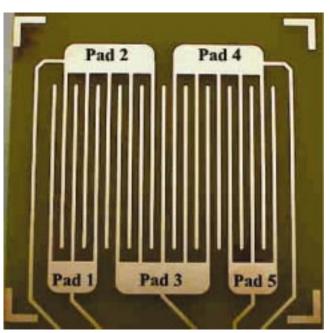


Figure 1

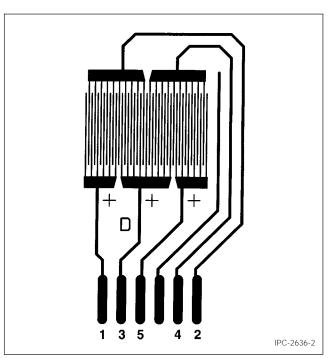


Figure 2

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When used for qualification purposes, the base laminate will be FR-4 epoxy-glass with 17 μm [0.5 oz equivalent] unprotected copper metalization.

4 Apparatus

4.1 A clean test chamber capable of producing and recording an environment of $35^{\circ}C \pm 2^{\circ}C$ [95°F $\pm 3.6^{\circ}F$] and 88% -0+5% relative humidity, and that allows the insulation resistance of the patterns to be measured under these conditions. The chamber must be capable of maintaining these conditions under load (i.e., with specimens in place).

4.2 Measuring equipment such as that described in ASTM D-257 with a range up to 10^{13} ohm and capable of yielding an accuracy of \pm 5% at 10^{12} ohm and an applied potential of 100 Vdc.

5 Test

5.1 Sample Sizes

- Three test patterns are produced for test with no applied solder mask and no applied flux (controls).
- Three test patterns are produced for test using the candidate material(s) and process(s).
- Sample preparation and enumeration shall also be in accordance with IPC-J-STD-004 ''SIR samples for Flux Qualification.''

5.2 Sample Identification Use a non-contamination method for identifying the test sample (e.g., vibrating scribe). During this process, handle the samples by the edges only or using non-contaminating gloves.

5.3 Wire Attach Cover the test patterns with noncontaminating film, such as aluminum foil or plastic film, to prevent flux spattering during the wire attach process. Use water white rosin (non-activated flux) or dry-solder (no flux at all) to solder PTFE-insulated wires to the connection points of the specimens. Do not attempt to remove the flux residues. Alternatively, connections may be made by mechanical pressure connections (e.g., alligator clips).

NOTE: Because of the very high resistance levels typically used as pass-fail criteria for this method, a connector-based or other fixtured setup is not recommended, due to leakage currents, unless these systems can be shown to have no signal degradation compared to hardwiring.

It is an option to pre-condition test samples for 24 hours at 23 $^\circ\text{C}$ [73 $^\circ\text{F}]$ and 50% R.H. before testing.

5.4 Placing in Chamber Place the specimens in the environmental chamber in a vertical position such that the airflow is parallel to the direction of the board in the chamber. Allow at least 1.25 cm [0.5 in] between each test sample. Dress all wiring away from the test patterns. Route the wires to the outside of the chamber. Set the chamber temperature to 35°C [95°F] and 85% minimum relative humidity, with a ramp time of not less than one hour. There is no electrical potential applied to any test pattern during the first 24 hours of test exposure.

5.5 Resistance Measurements After 24 hours of test exposure with no applied electrical potential, measure the insulation resistance of each pattern using an applied voltage of 100 ± 2 volts DC and an electrification time of 60 seconds.

NOTE: It is recommended that the temperature and humidity levels be verified to be within the recommended limits prior to beginning the resistance measurements.

Each comb pattern requires four test measurements. Measurements are made between (see Figure 1):

- Pad 1 to Pad 2
- Pad 3 to Pad 2
- Pad 3 to Pad 4
- Pad 5 to Pad 4

Pads 2 and 4 are at one potential and Pads 1, 3, and 5 are at ground potential (see Note 6.3).

Determine the means of the dataset as outlined in 5.6.

After the 24 hour measurements, apply a bias of 48 volts DC to all test patterns, using the same polarity as used for the resistance measurements.

After an additional 72 hours (96 hours total), repeat the measurement series using an applied voltage opposite in polarity to that of the conditioning bias.

Remove all bias from the test specimens and return the chamber to ambient conditions over a one hour period. Remove all samples from the chamber for visual examination.

5.6 Data Analysis The average insulation resistance for each sample group, taken at 24 hours and again at 96 hours, shall be greater than the minimum set forth in IPC-J-STD-004. The average insulation resistant (IR_{avo}) shall be defined as the

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geometric mean of the sample set and can be calculated from the following:

$$IR_{avg} = 10 \left[\frac{1}{N} \sum_{1}^{N} log_{10} (IR)_{i} \right]$$

Where:

N = Number of Test Points (12 nominal for each set of three patterns).

 IR_i = individual insulation resistance measurements (see 6.6 for an example).

No individual insulation resistance value may be more than a factor of 10 below the specified minimum value.

Where an assignable cause of low insulation resistance, which is properly attributable to the laminate itself, or to the process used to produce the PCB, can be found, then such a value can be excluded from calculating the average value, provided that at least 10 (of the original 12) test points are included in the average.

Such assignable causes include the following:

- Contamination on the insulating surface of the board, such as lint, solder splines or water droplets from the chamber.
- Incompletely etched patterns that decrease the insulating space between the conductors by more than the amount allowed in the appropriate design requirements drawing.
- Scratched, cracked, or obviously damaged insulation between conductors.

5.7 Visual Analysis Discoloration of the patterns (green, blue-green, blue, or blue-black coloration of the conductors) shall be considered a failure.

6 Notes

6.1 If condensation occurs on the test specimens in the environmental chamber while the samples are under voltage, dendritic growth will occur. This can be caused by a lack of sufficient control of the humidification of the oven. Water spotting may also be observed in some ovens where the airflow in the chamber is from back to front. In this case, water condensation on the cooler oven window can be blown around the oven as micro-droplets which deposit on test specimens and cause dendritic growth if the spots bridge the distance between two electrified conductors. Both of these conditions must be eliminated for proper testing.

6.2 Tight control of the test humidity is critical for this test method. A difference of 5% relative humidity can result in a

0.5 - 1.0 decade difference in the measured resistance. The uniformity of the environment is also important. A fully loaded chamber, where airflow is severely impeded, may have a 30-40% RH range within the chamber workspace.

6.3 The polarity of the applied voltage is not important as long as the application is consistent (e.g., Pads 1, 3, 5 are positive and 2, 4 are at ground potential, vs. Pads 2 and 4 positive, and Pads 1, 3, 5 at ground potential).

6.4 The 0.318 mm [0.0125 in] lines/space pattern can also be found on the obsolete IPC-B-25 standard test board. This board was re-designed for improved SIR measurement accuracy (better routing of traces) and carries the designation IPC-B-25A. Pattern D of the B-25A board is preferred over the B/E pattern of the IPC-B-25.

6.5 IR_{ave} is also referred to as the geometric mean of the data set. Most spreadsheet packages contain functions for calculating the geometric mean of a data set. If you are computing the geometric mean of a large dataset, the spreadsheet may come back with an error because the number is so large. In such cases, use the antilog of the LogOhm average to arrive at the geometric mean. See the following example.

6.6 Example of Numerical Calculations

Three 5-point test patterns (4 measurements each) LogOhms = base-10 logarithm of measured resistance

No.	Resistance (Ohms)	LogOhms
1	3.98E+11	11.60
2	1.58E+11	11.20
3	6.31E+11	11.80
4	7.94E+11	11.90
5	1.00E+12	12.00
6	1.00E+12	12.00
7	3.98E+11	11.60
8	1.58E+12	12.20
9	1.26E+12	12.10
10	1.26E+12	12.10
11	1.00E+12	12.00
12	3.98E+11	11.60

Average of LogOhms = 11.84

Antilog of LogOhm Average = 6.94E+11 ohms = Geometric Mean = IR_{ave}